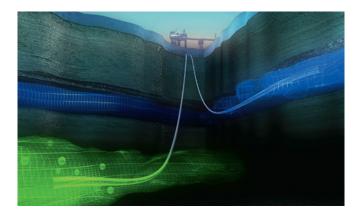
Mathematical Modeling Project fall 2019

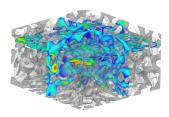
#### Underground CO2 Storage



#### Multiphase flow in porous media

- The rock is porous
- We displace a water phase by a CO2 phase.
- Multiphase flow in porous media





$$\begin{aligned} \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) &= 0\\ \frac{\partial \rho u}{\partial t} + \nabla \cdot (\rho u \otimes u) &= -\nabla p + \mu \Delta u + \frac{\mu}{3} \nabla (\nabla \cdot u) + f \end{aligned}$$



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$$\frac{\partial \rho u}{\partial t} + \nabla \cdot (\rho u \otimes u) = -\nabla p + \mu \Delta u + \frac{\mu}{3} \nabla (\nabla \cdot u) + f$$



Navier-Stokes equation

$$\nabla \cdot u = 0$$
$$\mu \Delta u - \nabla p + f = 0$$

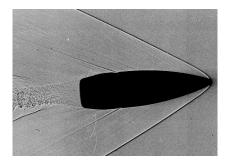


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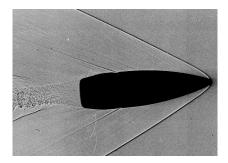


Incompressible Stokes equation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) = 0$$
$$\frac{\partial \rho u}{\partial t} + \nabla \cdot (\rho u \otimes u) = -\nabla p + f$$

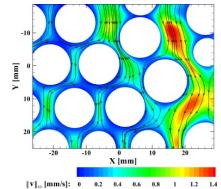


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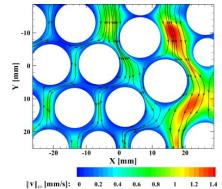


Euler equation

Strong variation of the velocity at the pore scale

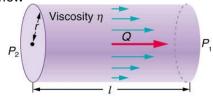


Strong variation of the velocity at the pore scale

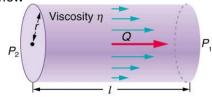


 We cannot approximate these oscillations. We use a velocity average or **Darcy velocity**.

Poisefeuille flow



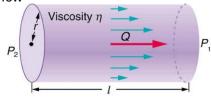
Poisefeuille flow



• We can compute the exact solution of the Stokes equation and obtain

$$\frac{Q}{\Delta P} = \frac{\pi R}{8\mu L}.$$

Poisefeuille flow



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$$\frac{Q}{\Delta P} = \frac{\pi R}{8\mu L}.$$

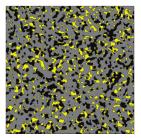
 By homogenization, we can show that there exist a permeability tensor K such that

$$u = -\frac{1}{\mu} \boldsymbol{K} \nabla p$$

for the Darcy's velocity u.

## Immiscible flow

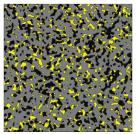
#### Immiscible phases



- black : solid part
- gray : wetting phase
- yellow : non-wetting phase

## Immiscible flow

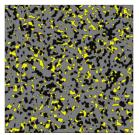
Immiscible phases



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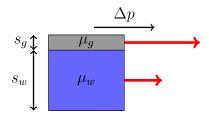
## Immiscible flow

Immiscible phases



- black : solid part
- gray : wetting phase
- yellow : non-wetting phase
- Again, we cannot track all these details.
- We use upscaled variable:
  - porosity :  $\phi$
  - saturation :  $s_g$  and  $s_w$ , volume fraction of the pore volume occupied by the phase

The Darcy's velocity is inversely proportional to the viscosity



## Surface tension and Young Laplace equation

Surface tension





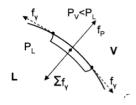
## Surface tension and Young Laplace equation

Surface tension





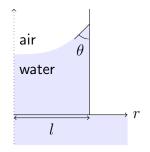
An interface can withstand a pressure



Young-Laplace equation

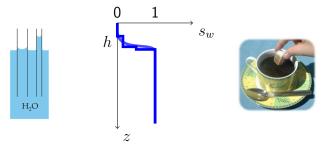
$$\Delta p = \gamma (\frac{1}{R_1} + \frac{1}{R_2})$$

- The shape of a meniscus is the result of force balance between
  - Gravity forces
  - Surface tension between air and water
  - Affinity between water/air and container.



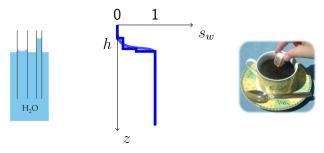
## Capillary effects - homogenization

• We cannot model the details. We proceed with **homogenization** 



## Capillary effects - homogenization

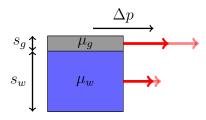
• We cannot model the details. We proceed with **homogenization** 



 The upscaled effects are given by the relative permeability and the capillary pressure function.

### relative permeability

• The relative permeability accounts for the difficulty of a phase to flow when it is surrounded by another phase.



In this case, it is **relatively harder** for the gas to flow in because there is a lot of water.

# Capillary pressure function

- One pressure per phase,  $p_g$  and  $p_w$
- The capillary function is a function of saturation which relates the two pressure phases,

$$p_c(s) = p_w - p_g$$

# Capillary pressure function

- One pressure per phase,  $p_g$  and  $p_w$
- The capillary function is a function of saturation which relates the two pressure phases,

$$p_c(s) = p_w - p_g$$

- Consider  $p_w$  as reference pressure. Then, the gas pressure is

$$p_g = p_w - p_c(s).$$

• Property:  $p_c$  is monotone decreasing.

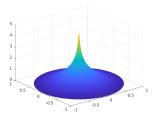
#### project description

## Single phase flow

Governing equation

$$\frac{\partial \rho \phi}{\partial t} + \nabla \cdot \left( -\frac{\rho}{\mu} \boldsymbol{K} \nabla p \right) = 0.$$

 Q1,2: Derive the equation and compute the solution for a linear or point injection well with radially symmetric boundary conditions.



#### Two-phase flow

Governing equation

$$\frac{\partial \rho_{\alpha} \phi s_{\alpha}}{\partial t} + \nabla \cdot (\rho_{\alpha} \boldsymbol{u}_{\alpha}) = 0,$$
$$\boldsymbol{u}_{\alpha} = -\frac{s_{\alpha}}{\mu_{\alpha}} \boldsymbol{K} \nabla p.$$

Q3: Derive the equation

## Two-phase flow

Governing equation

$$\begin{aligned} \frac{\partial \rho_{\alpha} \phi s_{\alpha}}{\partial t} + \nabla \cdot (\rho_{\alpha} \boldsymbol{u}_{\alpha}) &= 0, \\ \boldsymbol{u}_{\alpha} &= -\frac{s_{\alpha}}{\mu_{\alpha}} \boldsymbol{K} \nabla p. \end{aligned}$$

- Q3: Derive the equation
- Fractional flow formulation. In 1D and incompressible case, the equations can be written in the fractional flow formulation,

$$(\phi s)_t + (f(s)u)_x = 0.$$

Q4,5: Explain this derivation.

## Hyperbolic conservation laws

- General form of an hyperbolic conservation law in 1D

$$s_t + f(s)_x = 0$$

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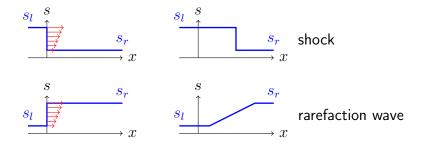
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- General form of an hyperbolic conservation law in 1D

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- Fundamental solutions for hyperbolic conservation laws are given by the **Riemann** problems
- Example: Burgers' equation:  $s_t + (s^2)_x = 0$ ,



## Fractional flow formulation

Governing equation

$$(\phi s)_t + (f(s)u)_x = 0$$

**Q5**: Compute the Riemann solution.

## Fractional flow formulation

Governing equation

$$(\phi s)_t + (f(s)u)_x = 0$$

Q5: Compute the Riemann solution.

• We add capillary pressure,  $p_c(s)$ .

$$(\phi s)_t + (f(s)u)_x - (g(s)s_x)_x = 0$$

**Q6,7**: Derive the equation. Find expressions for f and g. Solve the equation numerically.

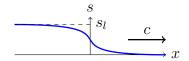
The equation

$$(\phi s)_t + (f(s)u)_x - (g(s)s_x)_x = 0$$

is no longer a hyperbolic conservation law. We do not have Riemann solution.

Q8: Investigate the existence of traveling waves,

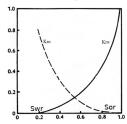
$$s(t,x) = \hat{s}(x - ct)$$



Find  $s_l$  and velocity c.

## Relative permeability

Relative permeabilities are empirical data

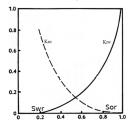


We have

$$u_{\alpha} = \frac{k_{r\alpha}(s_{\alpha})}{\mu_{\alpha}} K \nabla p$$

#### Relative permeability

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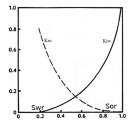
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$$u_{\alpha} = \frac{k_{r\alpha}(s_{\alpha})}{\mu_{\alpha}} K \nabla p$$

- The formulation allows for immobile oil or water
- Q9,10: What are the Riemann solutions and the traveling waves for the corresponding fractional flow formulation?

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$$\nabla_{\parallel} \cdot \left(\frac{k}{\mu} \nabla_{\parallel} P\right) = 0.$$

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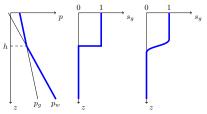
- This is a reduced model: The advantage is that a 3D problem becomes 2D. Easier to solve.
- **Q11,12**: Explain how the reduced model is obtained. Consider the compressible case.

• The phases segregate so that the gas remains at the top of the water

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- The vertical equilibrium equations (without capillary pressure) are

$$\lambda_{\alpha}(s_{\alpha})\frac{k}{\mu_{\alpha}}(\frac{\partial p}{\partial z}-\rho_{\alpha}g)=0,$$

• **Q13,14**: Compute the solution of the vertical equilibrium with and without capillary pressure



Governing equation for the reduced problem:

$$egin{aligned} &rac{\partial \phi S_lpha}{\partial t} + 
abla_{\parallel} \cdot oldsymbol{u}_lpha &= 0, \ &oldsymbol{u}_lpha &= -\Lambda_lpha(S_lpha)k
abla_{\parallel} P_lpha, \ &P_c(S_g) = P_w - P_g. \end{aligned}$$

Governing equation for the reduced problem:

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• Q15: Derive this model equation

Governing equation for the reduced problem:

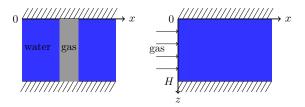
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- Q15: Derive this model equation
- Remarkably, the model equation takes the same form as the original 2D problem with relative permabilities and capillary pressure.

Fractional flow formulation

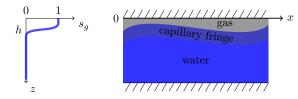
$$\frac{\partial \phi s}{\partial t} + \frac{\partial}{\partial x}(f(s)u - g(s)s_x) = 0.$$

 Q16,17: Derive fractional flow formulation. Implement numerical scheme. Solve for the following inputs

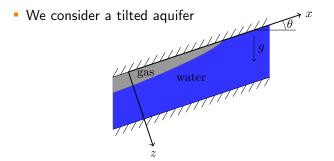


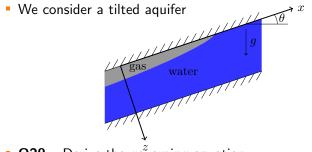
# Vertical Equilibrium Approximation - Capillary fringe

- We add capillary effects and obtain a capillary fringe



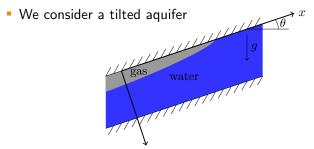
• **Q18,19**: Find a relation between  $S_g$  and h (where  $p_c(s_g(h)) = 0$ ). Derive the reduced model.





• **Q20**: Derive the governing equation  

$$\frac{\partial \phi s_{\alpha}}{\partial t} - \frac{\partial}{\partial x} (\lambda_{\alpha}(s_{\alpha})k(\frac{\partial p}{\partial x} + \rho_{\alpha}g\sin\theta)) - \frac{\partial}{\partial z} (\lambda_{\alpha}(s_{\alpha})k(\frac{\partial p}{\partial z} - \rho_{\alpha}g\sin\theta)) = 0$$

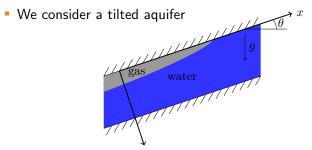


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Q21: Derive the reduced model and fractional flow formulation

$$\frac{\partial \phi s}{\partial t} + \frac{\partial}{\partial x} (f(s)u + g(s)(-H\cos\theta s_x + \sin\theta)) = 0$$



• Q20: Derive the governing equation

$$\frac{\partial \phi s_{\alpha}}{\partial t} - \frac{\partial}{\partial x} (\lambda_{\alpha}(s_{\alpha})k(\frac{\partial p}{\partial x} + \rho_{\alpha}g\sin\theta)) - \frac{\partial}{\partial z} (\lambda_{\alpha}(s_{\alpha})k(\frac{\partial p}{\partial z} - \rho_{\alpha}g\sin\theta)) = 0$$

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• Q22: Determine the traveling waves.

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- Questions!