

Uncertainty Quantification in Low Mach Number Reacting Flow Computations

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Motivation for Uncertainty Quantification (UQ)

- Rational model validation with respect to experimental measurements requires estimates of ranges of *error* in each set of data
- Experimental error-bars are (usually) available
- How large are the error bars on the computational results?
- Sources of error/uncertainty in the prediction
 - Model uncertainty
 - Parametric uncertainty
 - Numerical discretization errors
- Determining that numerical and experimental error bars do not overlap enables a decision on the efficacy of the *model* as distinct from the role of the *parameters*
- Focus on quantification of parameteric uncertainty (UQ)
 - in chemically reacting flow computations

Numerical Integration of Atmospheric Premixed CH₄-Air Flames

- H Diffusivity, $D_{\text{H,N}_2,1900\text{K}} \simeq 0.003 \text{ m}^2/\text{s}$
- Flame thermal thickness, $\delta_f \simeq 0.7 \text{ mm}$
- CH-radical profile FWHM in the reaction zone, $\delta_{\text{CH}} \simeq 100 \text{ }\mu\text{m}$
 - Necessary spatial resolution, $\Delta x \simeq 15\mu\text{m}$

- Convective CFL restriction

$$\frac{U_{\max}\Delta t}{\Delta x} < 1 \quad \Rightarrow \quad \Delta t < 1.5 \mu\text{s} \quad (U = 10 \text{ m/s})$$

- Explicit diffusion stability constraint in 2D

$$\frac{D_{\max}\Delta t}{\Delta x^2} < \frac{1}{4} \quad \Rightarrow \quad \Delta t < 20 \text{ ns}$$

- Chemical Stiffness, GRImech1.2 : $\Rightarrow \Delta t \leq 2 \text{ ns}$ (Explicit)

Low Mach Number Approximation

- Expand flow quantities in terms of $\epsilon = \gamma M^2$

$$p = p_0 + \epsilon p_1 + \epsilon^2 p_2 + \dots$$

- Take the limit as $M \rightarrow 0$, retain lowest order terms
- Generally accepted for $M < 0.3$, i.e. $M^2 < 0.1$
- Consequences
 - Neglects elastic compressibility of the fluid
 - The zeroth-order (in ϵ) momentum equations reduce to $\nabla p_0 = 0$
 - The dynamic pressure $p_1 = p_1(\mathbf{x}, t)$ survives in the ($\mathcal{O}(\epsilon)$) mom. eqs
 - The stagnation pressure $p_0 = p_0(t)$ survives in the state equation
 - The state equation couples ρ and p_0
 - Coupling of \mathbf{v} and ρ through the momentum equations and p is lost
 - Requires **both** low M^2 **and** fast acoustic time scales, vis. singing flames

Governing 2D Dimensionless Low Mach Number Equations

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0$$

$$\frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u^2)}{\partial x} + \frac{\partial(\rho uv)}{\partial y} = -\frac{\partial p}{\partial x} + \frac{1}{Re} \left[\frac{4}{3} \frac{\partial}{\partial x} \left(\mu \frac{\partial u}{\partial x} \right) - \frac{2}{3} \frac{\partial}{\partial x} \left(\mu \frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu \frac{\partial v}{\partial x} \right) \right]$$

$$\frac{\partial(\rho v)}{\partial t} + \frac{\partial(\rho vu)}{\partial x} + \frac{\partial(\rho v^2)}{\partial y} = -\frac{\partial p}{\partial y} + \frac{1}{Re} \Phi_y$$

$$\rho c_p \frac{DT}{Dt} = \frac{(\gamma - 1) dp_o}{\gamma dt} + \frac{1}{RePr} \nabla \cdot (\lambda \nabla T) - \frac{\rho}{ReSc} \sum_{i=1}^N c_{p,i} \mathbf{V}_i \cdot \nabla T - Da \sum_{i=1}^N h_i w_i$$

$$\frac{\partial(\rho Y_i)}{\partial t} + \nabla \cdot (\rho \mathbf{v} Y_i) = -\frac{1}{ReSc} \nabla \cdot (\rho Y_i \mathbf{V}_i) + Da w_i \quad i = 1, \dots, N$$

$$p_o = \frac{\rho T}{\overline{W}}$$

-
- 2D, Low Mach No., no body forces, no radiation.
 - Neglect Soret and Dufour effects
-

Intrusive Spectral Stochastic UQ Formulation

- Model uncertain parameters as random variables
- A stochastic process $u(\mathbf{x}, t, \theta)$ can be described by :
a Polynomial Chaos (PC) expansion in terms of Hermite polynomials Ψ_k ,
their associated Gaussian density $\xi(\theta)$,
and spectral mode strengths $u_k(\mathbf{x}, t)$

$$u(\mathbf{x}, t, \theta) = \sum_{k=0}^{\infty} u_k(\mathbf{x}, t) \Psi_k(\xi(\theta)) \simeq \sum_{k=0}^P u_k(\mathbf{x}, t) \Psi_k(\xi(\theta))$$

- Literature:

Wiener : 1938 : Homog. Chaos – span of Hermite pol. functionals of a Gaussian process

Cameron & Martin : 1947 : L^2 Convergence for any L^2 stochastic process

Ghanem & Spanos : 1991 : Application to UQ in Stochastic Finite Element Method

Le Maître *et al.* : 2001,2002 : Application to Fluid Flow

Xiu & Karniadakis : 2002 : Conv. rate for Gaussian/non-Gaussian processes

Debusschere *et al.* : 2003 : Application to electrochemistry in microfluid flow

Reagan *et al.* : 2003 : Application to reacting thermofluid flow

Intrusive Spectral Stochastic UQ Formulation: ODE Example

- Sample ODE with parameter λ :

$$\frac{du}{dt} = \lambda u, \quad u(0) = u_0$$

- Let λ be uncertain : Represent it as a stochastic quantity
 - Introduce a new dimension ξ , where ξ is a Normal random variable
 - Use P -th order Polynomial Chaos (PC) expansions:

$$\lambda = \sum_{k=0}^P \lambda_k \Psi_k(\xi), \quad u = \sum_{k=0}^P u_k \Psi_k(\xi), \quad (\lambda_k \text{ known, } u_k(t) \text{ unknown})$$

- The Ψ_k 's are orthogonal Hermite polynomials $\langle \Psi_i \Psi_j \rangle = \langle \Psi_i^2 \rangle \delta_{ij}$
- Substitute PC expansions for λ and u in the ODE, and reformulate:

$$\frac{du_i}{dt} = \sum_{p=0}^P \sum_{q=0}^P \lambda_p u_q C_{pqi}, \quad i = 0, 1, \dots, P$$

where the $C_{pqi} = \langle \Psi_p \Psi_q \Psi_i \rangle / \langle \Psi_i^2 \rangle$ are known coefficients.

Pros & Cons

- This intrusive spectral construction is potentially very efficient
 - N -dimensional **linear**: $du/dt = f(u)$, with M -gaussian parameters
 - * requires one solution of a $2N$ -dimensional linear system
 - Non-linearities and non-gaussian behaviour ... no general answer
- It allows the identification of individual contributions of model parameters to uncertainty in predictions
 - Highlights parameters where additional experimental measurements would have the greatest impact on improving the quality of predictions
- Significant complexity, model & numerics reformulation, code rewrite
- Non-linear chemical source terms may require high-order expansions
- Stability issues related to finite probabilities of negative concentrations
 - Hermite-polynomials and Normal ξ OK for weak nonlinearity
 - Need (non-Gaussian) ξ -basis with positive-support for chemistry
 - Laguerre-polynomials and Gamma-distributions may do well in flames

Chemical Source Term

- Complex and Expensive *Spectral* representation
 - Arrhenius rate expressions, thermodynamic properties, forward and reverse rates, third-body and pressure corrections
 - *Many*-dimensional expectation coefficients and summations
- Alternative *Pseudo-Spectral* technique
 - Simpler, Modular, Efficient
 - Projection of pair-wise products of n -order polynomials onto an n -order polynomial

Pseudo-Spectral Construction - 1

$$w = \lambda u^2 v, \quad u = \sum_{k=0}^P u_k \Psi_k, \quad \text{similarly for } \lambda \text{ \& } v$$

$$\text{Spectral : } w_i = \sum_{j=0}^P \sum_{k=0}^P \sum_{l=0}^P \sum_{m=0}^P \lambda_j u_k u_l v_m \frac{\langle \Psi_j \Psi_k \Psi_l \Psi_m \Psi_i \rangle}{\langle \Psi_i^2 \rangle}, \quad i = 0, \dots, P$$

Pseudo-Spectral: Project each product onto a $(P+1)$ -polynomial before proceeding further

$$\tilde{w} = uv \quad \Rightarrow \quad \tilde{w}_i = \sum_{j=0}^P \sum_{k=0}^P u_k v_j \frac{\langle \Psi_k \Psi_j \Psi_i \rangle}{\langle \Psi_i^2 \rangle}, \quad i = 0, \dots, P$$

$$\hat{w} = u\tilde{w} \quad \Rightarrow \quad \hat{w}_i = \sum_{j=0}^P \sum_{k=0}^P u_k \tilde{w}_j \frac{\langle \Psi_k \Psi_j \Psi_i \rangle}{\langle \Psi_i^2 \rangle}, \quad i = 0, \dots, P$$

$$w = \lambda \hat{w} \quad \Rightarrow \quad w_i = \sum_{j=0}^P \sum_{k=0}^P \lambda_k \hat{w}_j \frac{\langle \Psi_k \Psi_j \Psi_i \rangle}{\langle \Psi_i^2 \rangle}, \quad i = 0, \dots, P$$

Pseudo-Spectral Construction for Non-Polynomial Functions

- How to propagate PC expansions ($\{u_k\} \Rightarrow \{v_k\}$) through functions like

$$v = \frac{1}{u}, \quad v = \ln u, \quad \text{or} \quad v = e^u$$

- Use local polynomial approximations, e.g. Taylor series ? ... NO
 - Fragile
 - convergence issues
 - high-order PC multiplications
 - instabilities

Inversion and division can be done without Taylor series.

- Assume three stochastic variables a , b , and c

$$c = \frac{a}{b} \Rightarrow b \cdot c = a$$

- Mode k of stochastic product $a = b \cdot c$

$$\sum_{m=0}^P \sum_{l=0}^P C_{klm} b_l \cdot c_m = a_k$$

- System of $P + 1$ linear algebraic equations in c_m with known a_k and b_l ,

$$B_{km} = \sum_{l=0}^P C_{klm} b_l, \quad \mathbf{Bc} = \mathbf{a}$$

- Solve using GMRES, or your favorite linear solver
- More robust than Taylor series expansion for $1/u$
- What about the condition number of \mathbf{B} ?

Integration approach for non-polynomial functions — (1)

- Require: $u = u(x)$ with $\dot{u} = du/dx$ being a rational function of u and/or x
- For $x \in \mathbb{R}$, $u \in \mathbb{R}^{\mathbb{R}}$, u is the solution of the ODE : $du/dx = \dot{u}$

$$du = \dot{u} dx$$

$$u(x_b) - u(x_a) = \int_{x_a}^{x_b} \dot{u} dx$$

- Then, let x, u , and $v = \dot{u}$ be given by their PC expansions,

$$x(s, \theta) = \sum_{i=0}^P x_i(s) \Psi_i(\theta), \quad u(s, \theta) = \sum_{i=0}^P u_i(s) \Psi_i(\theta), \quad v(s, \theta) = \sum_{i=0}^P v_i(s) \Psi_i(\theta)$$

where s parameterizes the evolution of the spectral mode strengths along a path in the x -space from x_a to x_b .

Integration approach for non-polynomial functions — (2)

Then

$$\frac{\partial u}{\partial s}\Big|_{\theta} = v \frac{\partial x}{\partial s}\Big|_{\theta}, \quad \text{and} \quad \int_{s_a}^{s_b} \frac{\partial u}{\partial s}\Big|_{\theta} ds = \int_{s_a}^{s_b} v \frac{\partial x}{\partial s}\Big|_{\theta} ds$$

where

$$\frac{\partial u}{\partial s}\Big|_{\theta} = \sum_{i=0}^P \frac{du_i}{ds} \Psi_i$$
$$\frac{\partial x}{\partial s}\Big|_{\theta} = \sum_{i=0}^P \frac{dx_i}{ds} \Psi_i$$

and, substituting above

$$\sum_{i=0}^P \Psi_i \int_{s_a}^{s_b} \frac{du_i}{ds} ds = \int_{s_a}^{s_b} \left(\sum_{i=0}^P v_i \Psi_i \right) \left(\sum_{j=0}^P \frac{dx_j}{ds} \Psi_j \right) ds$$

or

$$\sum_{i=0}^P \Psi_i (u_i(s_b) - u_i(s_a)) = \sum_{j=0}^P \int_{s_a}^{s_b} \sum_{i=0}^P \Psi_i \Psi_j v_i \frac{dx_j}{ds} ds$$

Integration approach for non-polynomial functions — (3)

Then, apply Galerkin projection on the k -th mode,

$$u_k(s_b) - u_k(s_a) = \sum_{j=0}^P \int_{s_a}^{s_b} \sum_{i=0}^P C_{ijk} v_i \frac{dx_j}{ds} ds$$

Consider the integral :

$$I_{jk} = \int_{s_a}^{s_b} \sum_{i=0}^P C_{ijk} v_i \frac{dx_j}{ds} ds$$

Since $v = v(u(x), x)$, then $v_i = v_i(x) = v_i(x_0, x_1, \dots, x_P)$. In the evaluation of I_{jk} , only one x -coefficient, x_j is varied, while $x_{r \neq j}$ are constant. Thus, in this context, $v_i = v_i(x_j; x_{r \neq j}) = v_i(x_j)$, such that

$$I_{jk} = \int_{x_j(s_a)}^{x_j(s_b)} \sum_{i=0}^P C_{ijk} v_i dx_j$$

and

$$u_k(s_b) - u_k(s_a) = \sum_{j=0}^P \int_{x_j(s_a)}^{x_j(s_b)} \sum_{i=0}^P C_{ijk} v_i dx_j$$

Integration approach for non-polynomial functions — (4)

Thus

$$u_k(x_b) - u_k(x_a) = \sum_{j=0}^P \int_{(x_a)_j}^{(x_b)_j} \sum_{i=0}^P C_{ijk} (\dot{u})_i dx_j$$

- To evaluate $u(x)$, $x = \sum_{k=0}^P x_k \Psi_k$, $u = \sum_{k=0}^P u_k \Psi_k$,
 - use an initial condition x_a such that $u(x_a)$ is known
... e.g. $x_a = x_0 \in \mathbb{R}$, and $u(x_a) = u(x_0) = u_0 \in \mathbb{R}$, $u_{k>0}(x_a) = 0$
 - express $\dot{u} = du/dx = f(u, x)$, where f is a rational function
... ensures that $(\dot{u})_k$ are readily found from the known u_k and x_k coeffs at each integration step
- ok for e^x , e^{x^2} , and $\ln(x)$, with $\dot{u} = u$, $2xu$, and $1/x$ resp.
 - but not for $e^{\sin(x)}$, with $\dot{u} = u \cos(x)$
- Increased accuracy and robustness compared to Taylor series expansions
- Agrees well with directly-sampled PDFs
 - if PC order is high enough to accurately describe solution statistics

Spectral UQ Formulation: Incompressible Flow – Stochastic Projection Method

- Formulation:

$$\frac{\partial u_q}{\partial t} + \sum_{j,k=0}^P C_{jk} C_{jkq} = -\frac{\partial p_q}{\partial x} + \frac{1}{Re} \sum_{i,j=0}^P \mathcal{D}_{ij} C_{ijq}, \quad (1D)$$

$$\frac{\partial v_q}{\partial t} = C_q - \nabla p_q + D_q, \quad 2D : v = (u, v)$$

- Projection: for $q = 0, \dots, P$:

$$\begin{aligned} \frac{\tilde{v}_q - v_q^n}{\Delta t} &= C_q^n + D_q^n \\ \nabla^2 p_q &= \frac{-1}{\Delta t} \nabla \cdot \tilde{v}_q \\ \frac{v_q^{n+1} - \tilde{v}_q}{\Delta t} &= -\nabla p_q \end{aligned}$$

- $P + 1$ *decoupled* Poisson Equation solutions for the pressure modes.

Laminar 2D Channel Flow with Stochastic Viscosity

- Incompressible flow
- Gaussian viscosity PDF

$$- \nu = \nu_0 + \nu_1 \xi$$

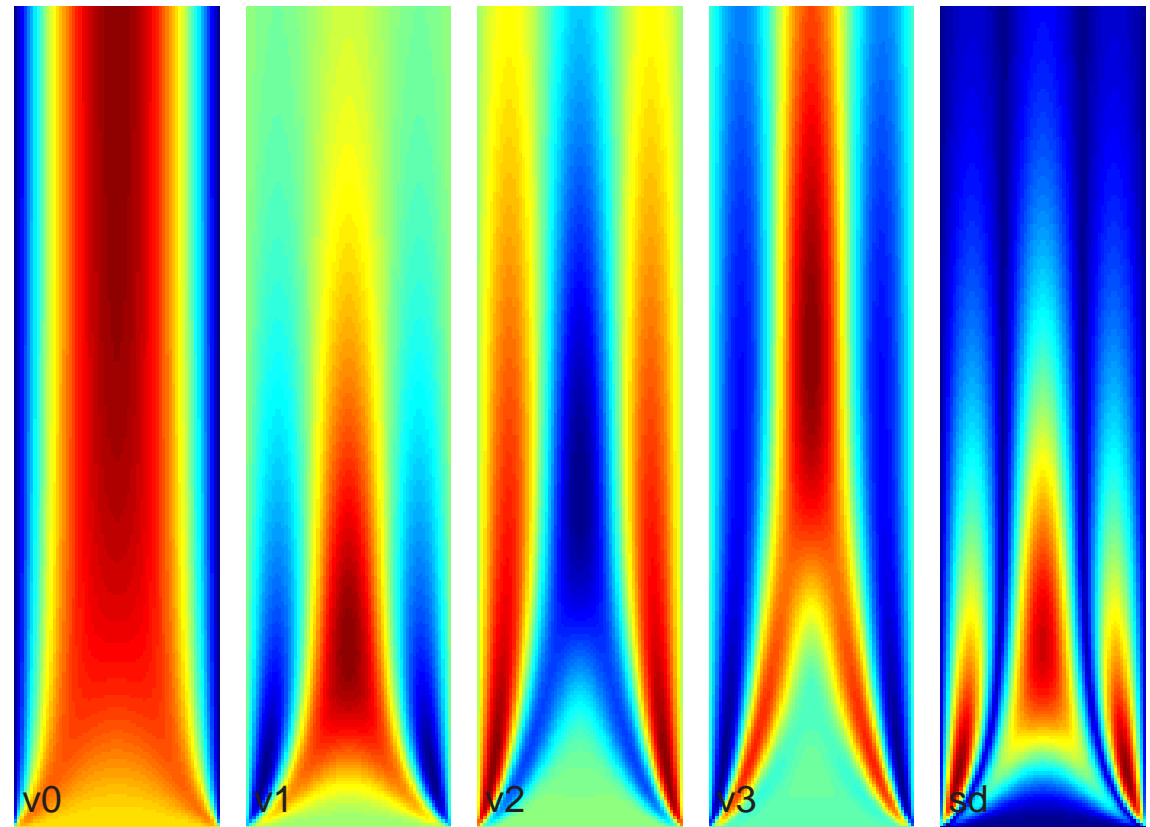
- Streamwise velocity

$$- v = \sum_{i=0}^P v_i \Psi_i$$

– v_0 : mean

– v_i : i -th order mode

$$- \sigma = \sqrt{\sum_{i=1}^P v_i^2 \langle \Psi_i^2 \rangle}$$



v_0

v_1

v_2

v_3

σ

Spectral UQ Formulation: low M 2D Momentum Equations

$$\frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u^2)}{\partial x} + \frac{\partial(\rho uv)}{\partial y} = -\frac{\partial p}{\partial x} + \frac{1}{Re} \left[\frac{4}{3} \frac{\partial}{\partial x} \left(\mu \frac{\partial u}{\partial x} \right) - \frac{2}{3} \frac{\partial}{\partial x} \left(\mu \frac{\partial v}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu \frac{\partial v}{\partial x} \right) \right]$$

$$u = \sum_{k=0}^P u_k \Psi_k, \quad v = \sum_{k=0}^P v_k \Psi_k, \quad \rho = \sum_{k=0}^P \rho_k \Psi_k, \quad p = \sum_{k=0}^P p_k \Psi_k, \quad \mu = \sum_{k=0}^P \mu_k \Psi_k$$

$$U = \rho u = \sum_{k=0}^P U_k \Psi_k, \quad C_{ijkq} = \frac{\langle \Psi_i \Psi_j \Psi_k \Psi_q \rangle}{\langle \Psi_q^2 \rangle}, \quad C_{ijq} = \frac{\langle \Psi_i \Psi_j \Psi_q \rangle}{\langle \Psi_q^2 \rangle}$$

$$\frac{\partial U_q}{\partial t} + \sum_{i,j,k=0}^P \left[\frac{\partial(\rho_i u_j u_k)}{\partial x} + \frac{\partial(\rho_i u_j v_k)}{\partial y} \right] C_{ijkq} = -\frac{\partial p_q}{\partial x} + \frac{1}{Re} \sum_{i,j=0}^P \left[\frac{4}{3} \frac{\partial}{\partial x} \left(\mu_i \frac{\partial u_j}{\partial x} \right) - \frac{2}{3} \frac{\partial}{\partial x} \left(\mu_i \frac{\partial v_j}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu_i \frac{\partial u_j}{\partial y} \right) + \frac{\partial}{\partial y} \left(\mu_i \frac{\partial v_j}{\partial x} \right) \right] C_{ijq}$$

Spectral UQ Formulation: Species Conservation Equation

$$\frac{\partial(\rho Y_i)}{\partial t} = -\nabla \cdot (\rho \mathbf{v} Y_i) + \frac{1}{Re Sc} \nabla \cdot (\rho D_i \nabla Y_i) + Da w_i, \quad i = 1, \dots, N$$

$$\rho = \sum_{k=0}^P \rho_k \Psi_k, \quad Y_i = \sum_{k=0}^P \rho_k \Psi_k, \quad \mathbf{v} = \sum_{k=0}^P \mathbf{v}_k \Psi_k, \quad D_i = \sum_{k=0}^P D_{i,k} \Psi_k, \quad w_i = \sum_{k=0}^P w_{i,k} \Psi_k$$

$$R_i = \rho Y_i = \sum_{k=0}^P R_{i,q} \Psi_q$$

$$\frac{\partial R_{i,q}}{\partial t} = - \sum_{j,k,p=0}^P \left[\nabla \cdot (\rho_j \mathbf{v}_k Y_{i,p}) + \frac{1}{Re Sc} \nabla \cdot (\rho_j D_{i,k} \nabla Y_{i,p}) \right] C_{jkpq} + Da w_{i,q}$$

$(q = 0, \dots, P. \quad i = 1, \dots, N)$

- Explicit Operator-Split transport terms integration
- Implicit chemical source term integration: $N(P + 1)$ coupled ODEs

Non-intrusive Spectral (NIS) UQ Formulation

- Construct spectral stochastic descriptions of uncertain parameters λ
- Sample parameter space and compute Monte-Carlo (MC) realizations of the deterministic model $u^i(t)$, $i = 1, \dots, N$
- Project MC statistics on the spectral mode strengths $u_k(t)$

$$u_k = \frac{\langle u \Psi_k \rangle}{\langle \Psi_k^2 \rangle}, \quad k = 0, \dots, P$$

- Sacrifices efficiency for reduced complexity *and* stability
 - May require excessively large number of samples to converge
- Retains spectral sensitivity information
- Allows designing UQ wrappers around legacy code

Sampling Issues in Non-Intrusive Spectral (NIS) Uncertainty Quantification (UQ)

- Need to minimize the number of samples required for evaluating spectral mode strengths
- Collocation techniques (DEMM, SRSM)
 - Minimize errors at sample points
 - High efficiency : number of samples \sim number of unknowns
- Galerkin projection (NISP)
 - Minimize RMS error
 - Less efficient but potentially more robust to nonlinearities
 - Projection is a Quadrature operation - samples are quadrature points
 - * Latin Hypercube Sampling
 - * Gauss-Hermite Quadrature
 - * Sparse Quadrature / Cubature

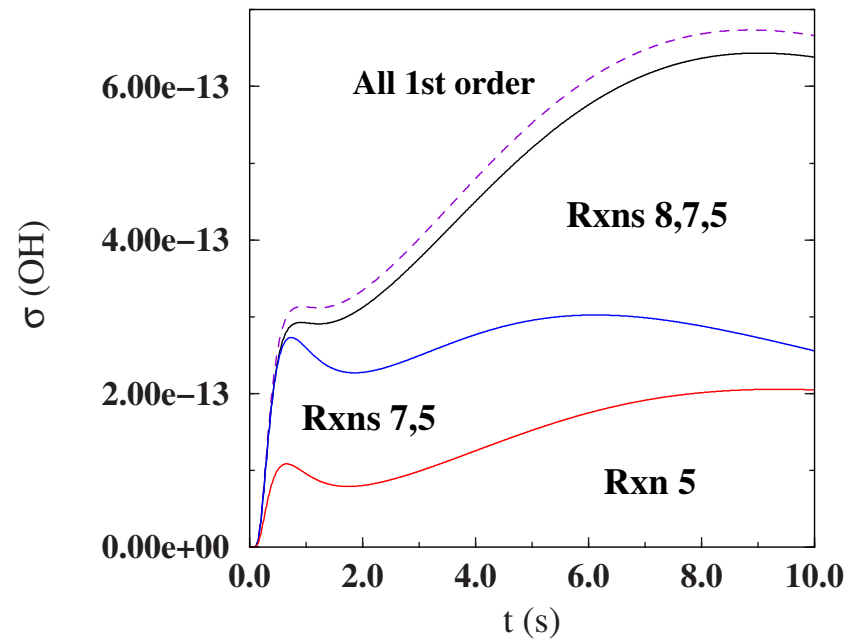
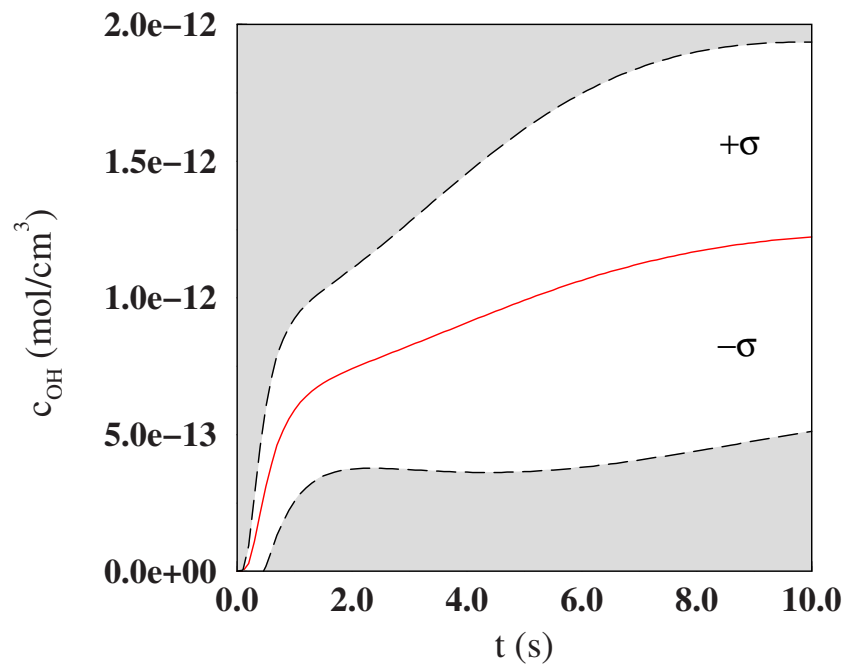
NISP UQ Application: 0D/1D Premixed H₂-O₂ at Super-Critical Water Oxidation (SCWO) Conditions

- Allow uncertainties in reaction rate constants and thermodynamic properties, per published experimental data
- Wrap NIS processing around a deterministic reacting flow code
- Using 8-step simplified SCWO Hydrogen mechanism (McRae)

Reaction	A	n	E_a/R	UF
1. OH + H ↔ H ₂ O	1.620E+14	0	75	3.16
2. H ₂ + OH ↔ H ₂ O + H	1.024E+08	1.6	1660	1.26
3. H + O ₂ ↔ HO ₂	1.481E+12	0.6	0	1.58
4. HO ₂ + HO ₂ ↔ H ₂ O ₂ + O ₂	1.867E+12	0	775	1.41
5. H ₂ O ₂ + OH ↔ H ₂ O + HO ₂	7.829E+12	0	670	1.58
6. H ₂ O ₂ + H ↔ HO ₂ + H ₂	1.686E+12	0	1890	2.00
7. H ₂ O ₂ ↔ OH + OH	3.0000E+14	0	24400	3.16
8. OH + HO ₂ ↔ H ₂ O + O ₂	2.891E+13	0	-250	3.16

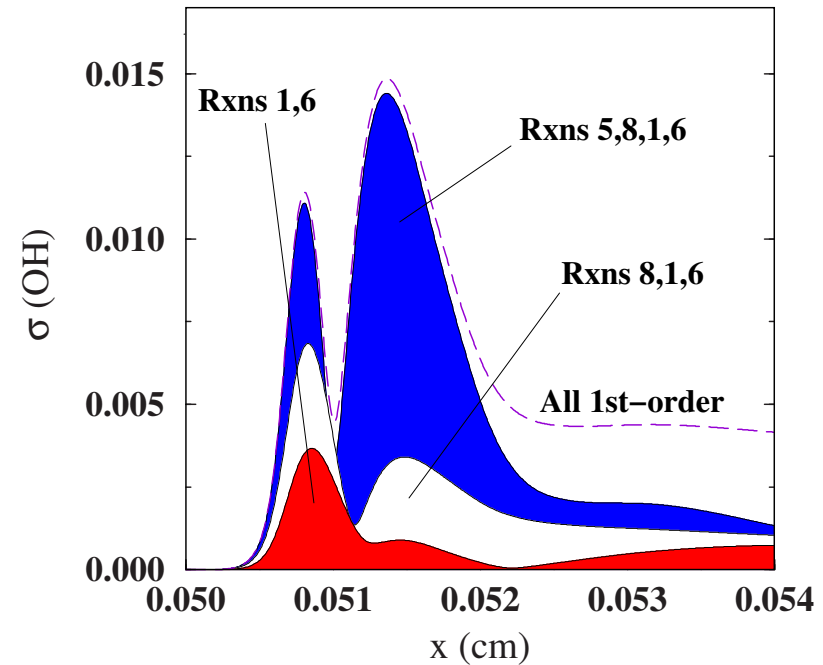
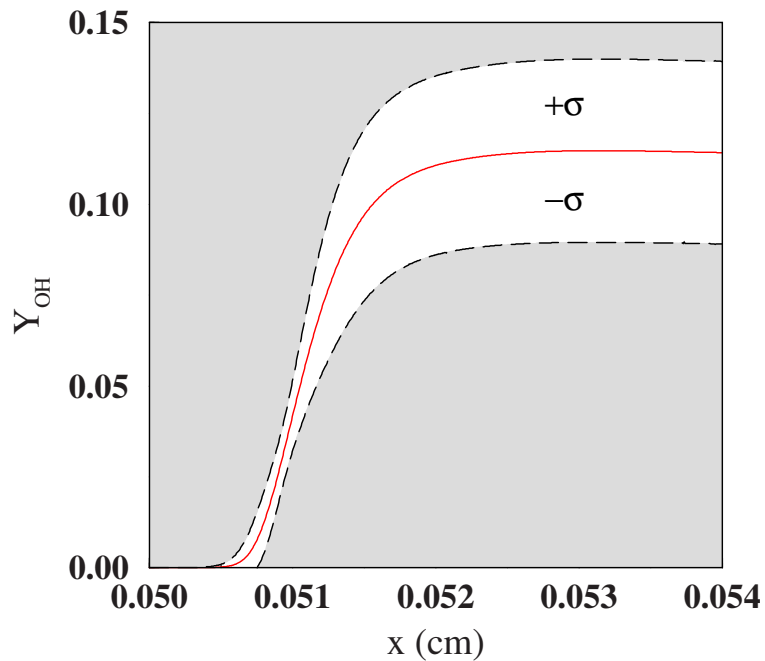
Species	μ_0	2σ
H	52.10	0.01
OH	9.3	0.2
H ₂ O	-57.80	0.01
H ₂ O ₂	-32.53	0.07
HO ₂	3.0	0.5

0D H₂-O₂ SCWO Ignition



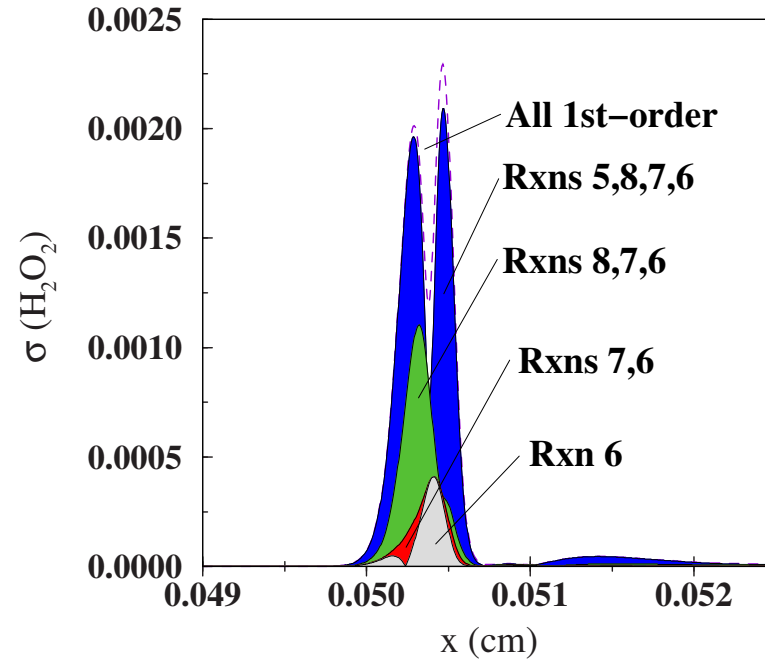
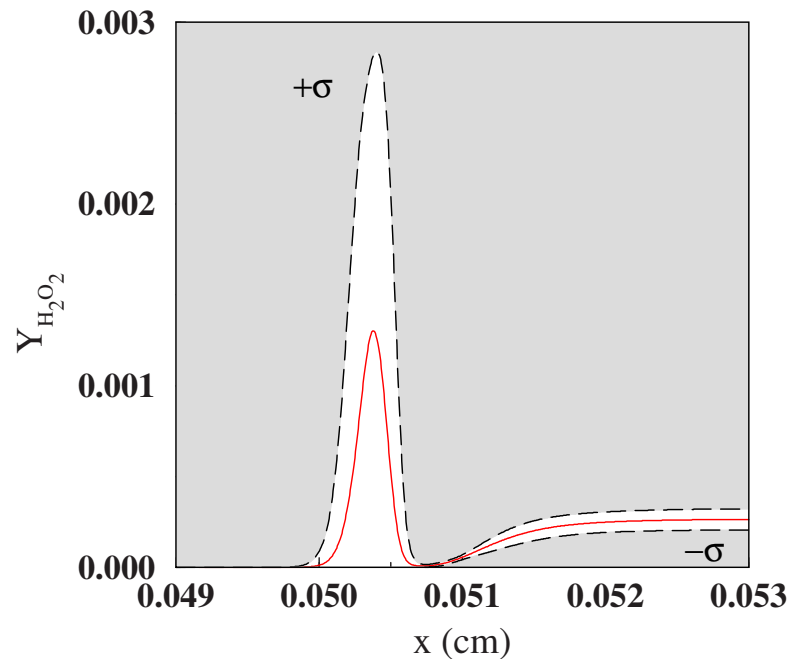
- Mean and standard deviation predictions validated against published data
- Initial fast growth in uncertainty followed by a slower approach to a steady-state with *large* OH uncertainty
- Reactions 7 & 8 have dominant roles in the OH uncertainty

1D H₂-O₂ SCWO Flame NISP UQ/Chemkin-Premix



- 1D freely propagating H₂-O₂ flame at SCWO conditions
- Fast growth in OH uncertainty in the primary reaction zone
- Steady level of uncertainty and mean of OH in the post-flame region
- Uncertainty in pre-exponential of Rxn.5 (H₂O₂+OH=H₂O+HO₂) has largest contribution to uncertainty in the predicted OH field

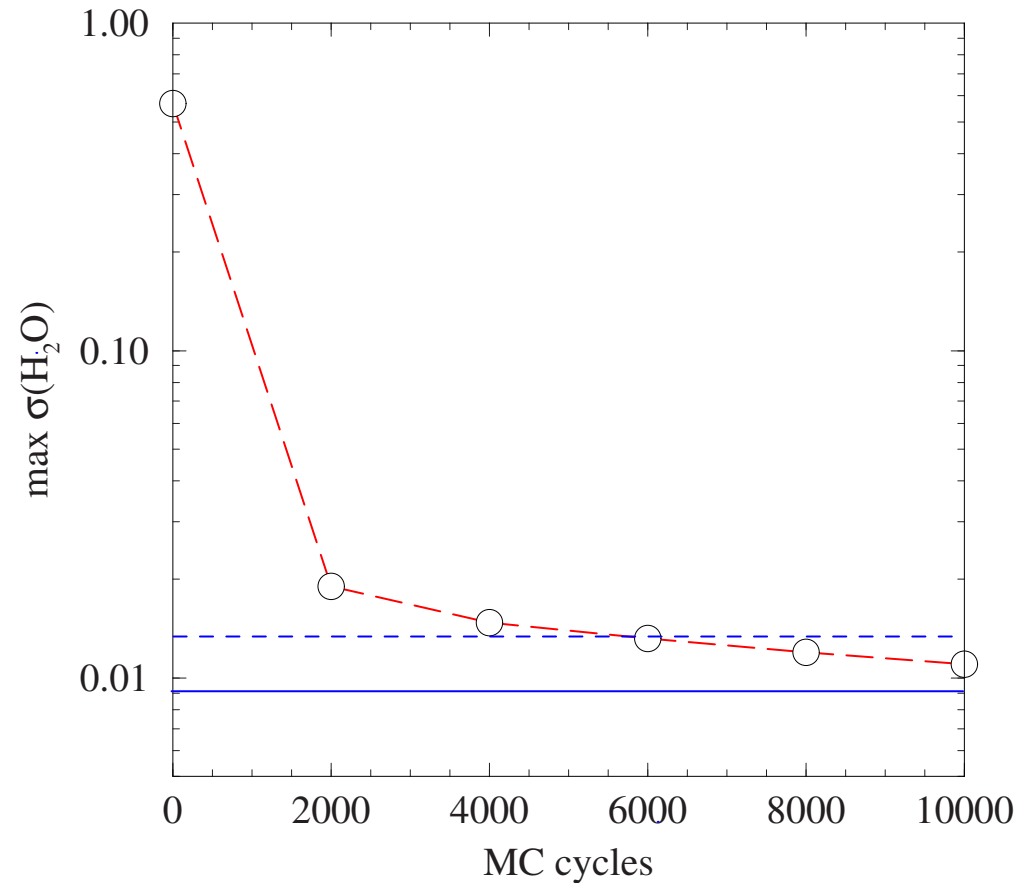
1D H₂-O₂ SCWO Flame NISP UQ/Chemkin-Premix



- Very large uncertainty in H₂O₂ prediction, $COV = \sigma/\mu = 100\%$!!
- Dominant source is again Rxn.5 ($H_2O_2 + OH = H_2O + HO_2$)
- Not a robust model for predicting H₂O₂ under SCWO conditions
- Results highlight the utility of additional experimental measurements of A_5

CPU-time Savings with Intrusive Spectral Strategy

- 0D H₂-O₂ SCWO ignition
- NISP standard deviation tends to that from the intrusive construction
- NISP comes to within 50% of the intrusive value after 6000 Latin-Hypercube realizations
- 6000 sample runs \sim 48 CPU hrs
- 1 intrusive run \sim 2 hrs



Experience with Instabilities

- When integrating a chemical system, e.g. ignition or 1D flame, regions of explosive mode growth (positive eigenvalues) can lead to instabilities.
- Instability manifested in the fast growth of higher order modes, and fast drift of the solution towards unphysical values
- Resulting fast rate of growth leads to failure due to finite arithmetic precision
- Adaptive stiff integrator (e.g. DVODE) unable to keep up the integration
- Typically occurs when the standard deviation increases significantly, becoming a sizeable fraction of the mean.
- Increasing PC order does not help much

A Study of *Intrusive* UQ Instabilities using a Model Problem

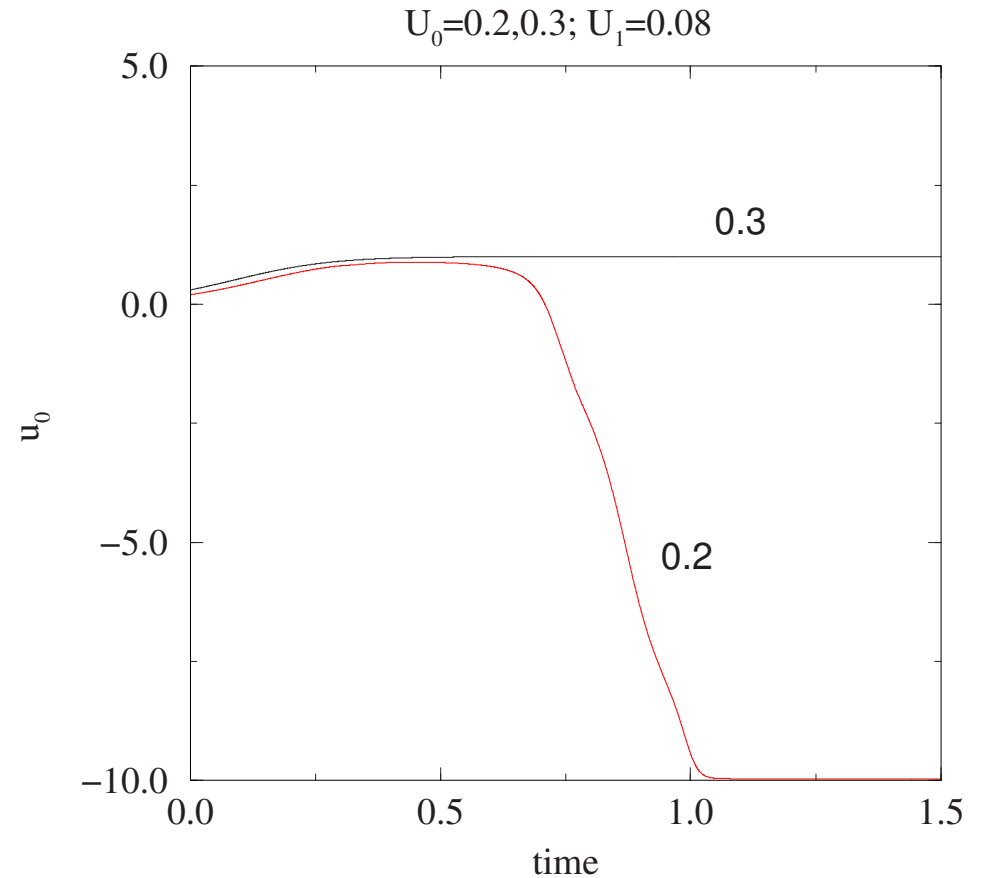
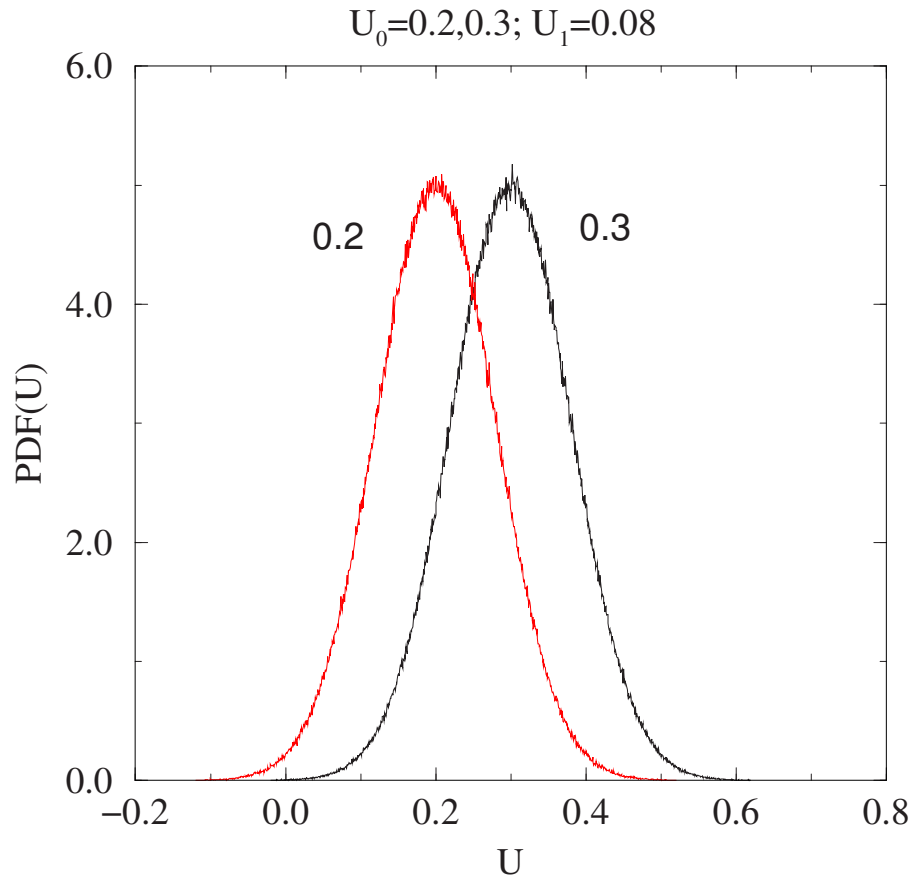
- Does the truncation of the PC expansion at P , and the resulting truncation error, lead to numerical instabilities akin to aliasing of unresolved high wavenumber energy in finite difference discretizations, and corruption of low wavenumber modes?
- Is a minimum spectral mode strength decay rate necessary for stability?
- Consider a model problem

$$\frac{du}{dt} = u(u + 10)(1 - u)$$

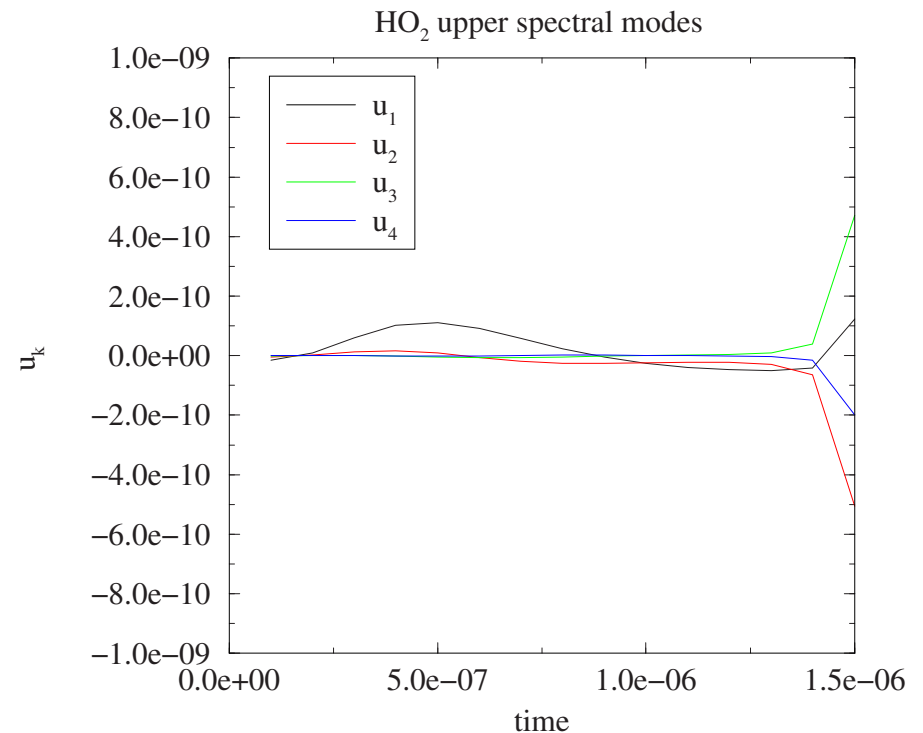
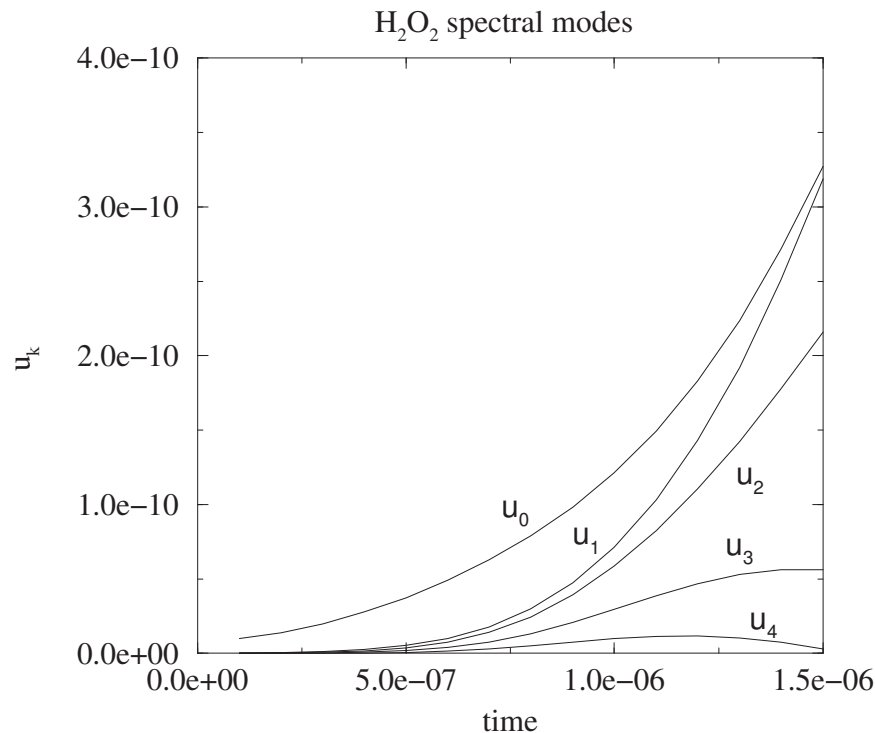
Attractors at $u = -10$, $u = 1$, and a repulsive fixed point at $u = 0$.

- Let the initial condition $u(t = 0) = U$ be stochastic, $U = \sum_{k=0}^P U_k \Psi_k$.
- Integrate the reformulated chaos system for the time evolution of u_k , $k = 0, \dots, P$, using DVODE

Model Problem: Two Finite Attractors: Consequence of Initial PDF tail zero crossing

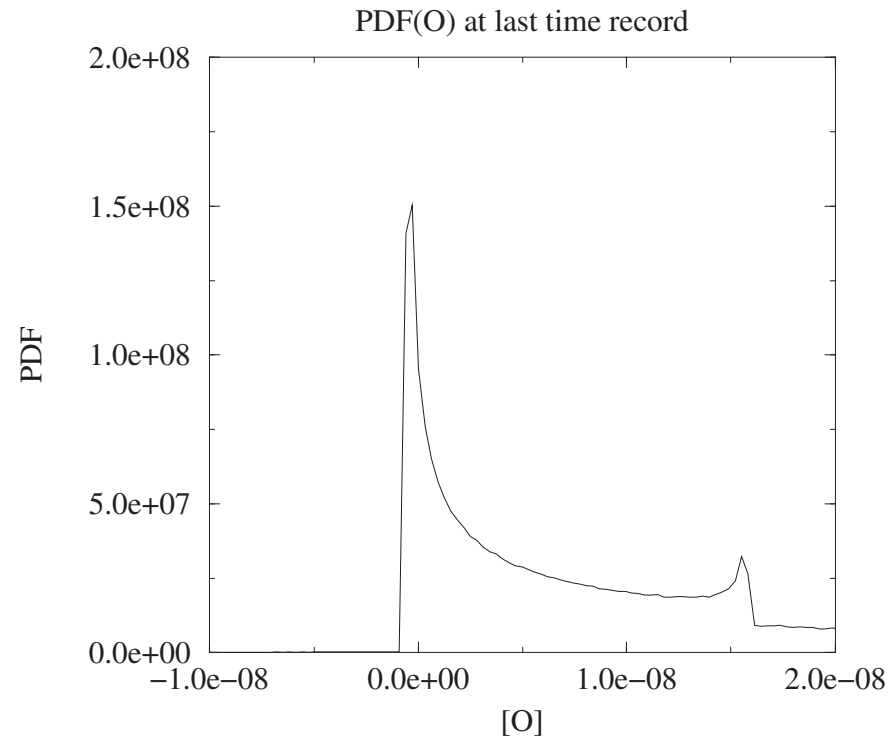


Ignition Instability — (1)



- Blowup occurs as u_1 approaches u_0 .
- Large rates of change observed in higher order modes.
- Problem is typically observed when the computed PC expansions of physical quantities (e.g. ρ, T, Y_i) correspond to PDFs with significant probability of negative values.

Ignition Instability — (2)



- PDF of [O] exhibits significant probability of non-physical negative values
- Finite probability of zero values of ρ would lead to ill-conditioned stochastic inversion matrices for $T = 1/\rho$

Summary

- UQ analysis is necessary for validation and improved understanding of the robustness and reliability of reacting flow models
- Spectral stochastic techniques offer significant efficient analysis capabilities allowing a detailed understanding of the role of each uncertain parameter in the model
- These techniques have been demonstrated in non-reacting and reacting 0D/1D/2D low Mach number flows
- Intrusive/non-intrusive versions provide requisite sensitivity information
 - Intrusive construction was found to be *much* more efficient than the non-intrusive MC-based approach, for 0D ignition
- Non-linearities of chemical source terms offers challenges as regards the growth of uncertainty, bifurcation, etc, for *large* uncertainties in parameters
- Investigate alternative bases, e.g. Laguerre-Gamma